



UFPR-DELT
Programa de Pós Graduação em
Engenharia Elétrica

Integridade de Sinais Elétricos

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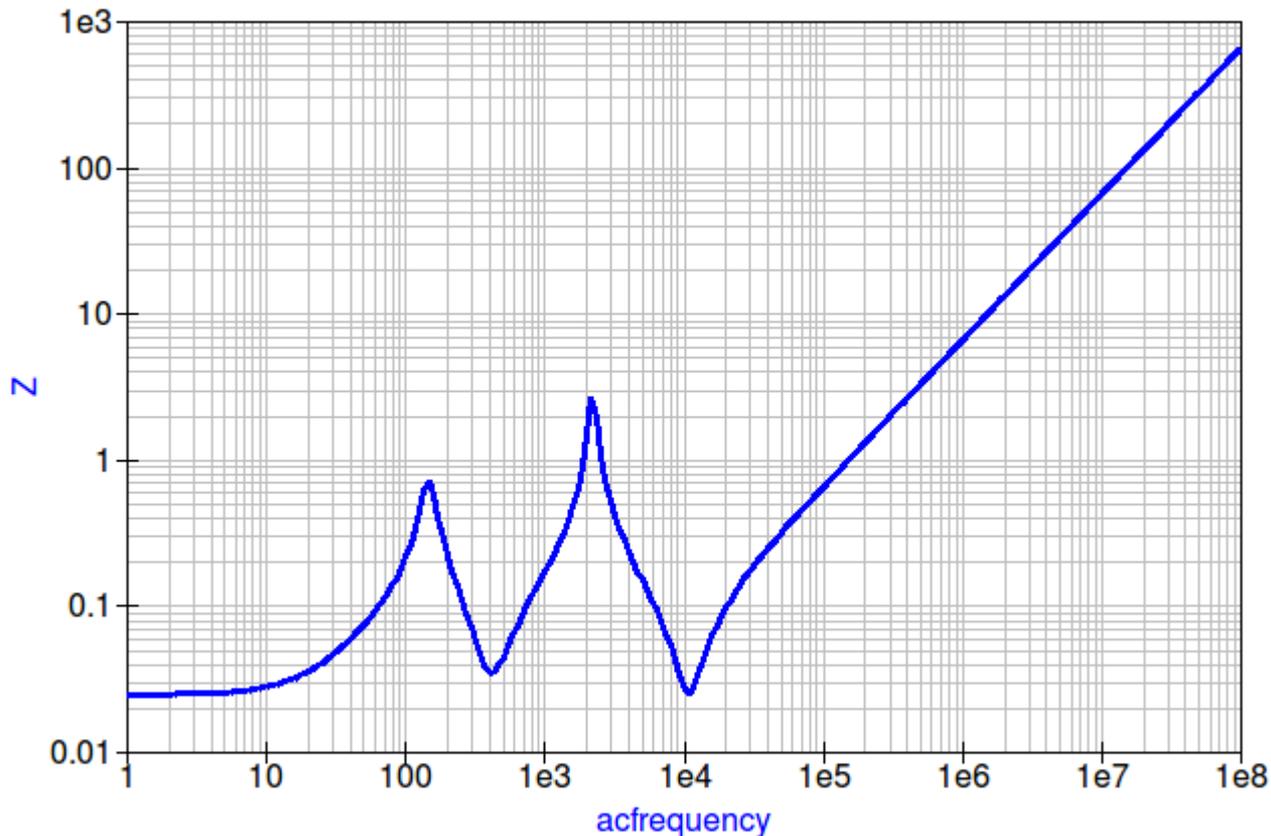
1º semestre 2012

Problemas associados à alimentação de circuitos

- Fontes de alimentação (tensão) ideais possuem impedância nula em qualquer frequência
- Fontes de alimentação reais possuem impedância variável com a frequência
- Impedância da fonte é dominada por:
 - Baixas frequências (0 – 100 Hz): circuito de realimentação
 - Médias frequências (100 – 10 kHz): capacitores de filtro
 - Altas frequências (> 10 kHz): Indutância das conexões

Problemas associados à alimentação de circuitos

Impedância típica de fonte de alimentação regulada

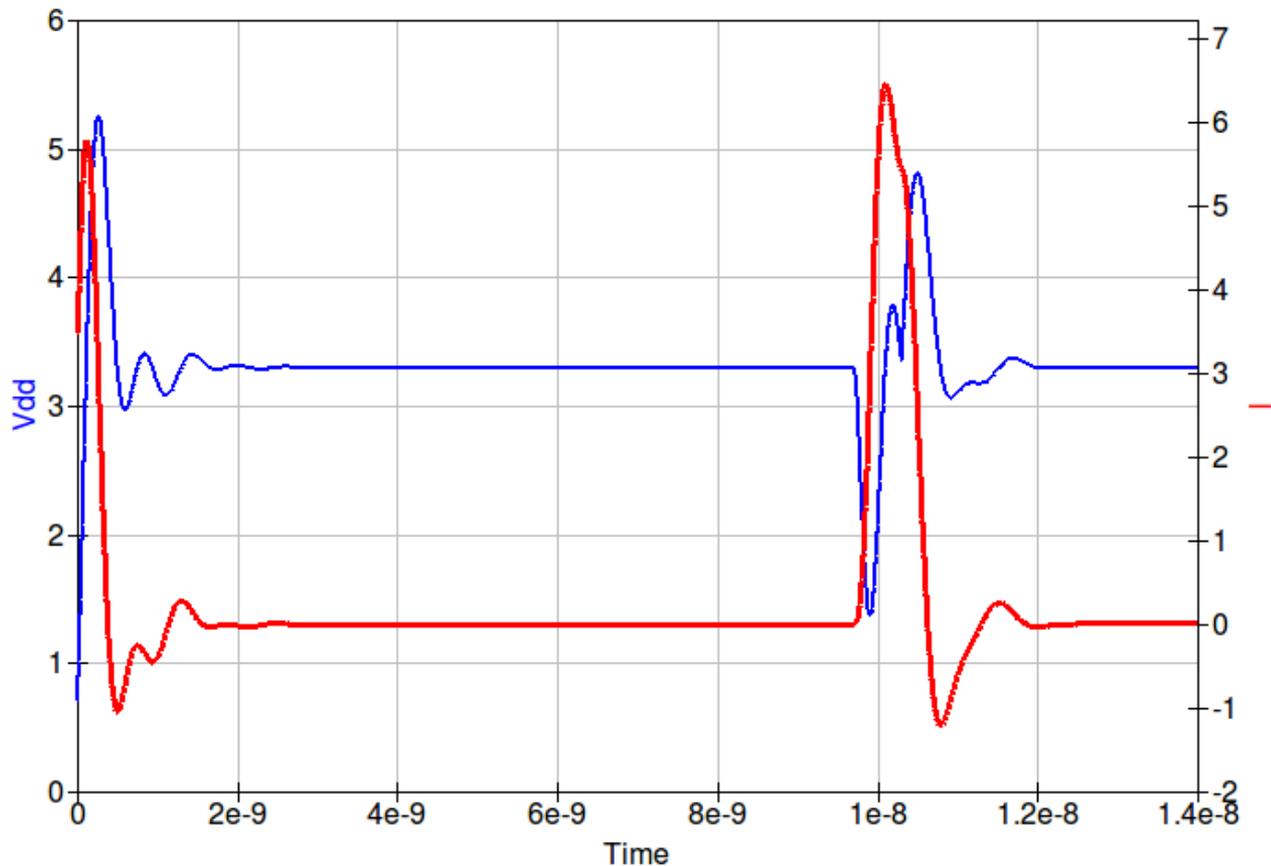


Problemas associados à alimentação de circuitos

- Circuitos de alta frequência geram transientes de corrente na sua alimentação
- Em particular os circuitos digitais CMOS geram transientes de corrente nas transições de nível lógico
- Um microprocessador atual chega a gerar transientes de corrente de centenas de Ampères em alguns ns
- Estes transientes de corrente geram variações rápidas na tensão de alimentação (ruídos)
- Ruídos na alimentação são grandes fontes de erro em circuitos digitais e de altas frequências e devem ser minimizados

Problemas associados à alimentação de circuitos

Tensão e corrente na alimentação de um circuito digital CMOS



Problemas associados à alimentação de circuitos

- Capacitores de filtro da alimentação são essenciais em circuitos de alta frequência
- Devem ser colocados o mais próximo possível dos circuitos para minimizar o efeito das indutâncias de conexão
- Deve-se levar em conta as não idealidades dos capacitores (indutância e resistência série)
- De modo geral são necessários vários capacitores em paralelo para atingir os objetivos de filtragem adequada
- O projeto destes capacitores leva em conta a impedância máxima permitida em determinada faixa de frequência ou o ruído máximo

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We will begin in

minutes

No Myths Allowed Webinar Series

NMA-840

Dec 9, 2009

Selecting Capacitors for the PDN

Eric Bogatin,

Signal Integrity Evangelist, Bogatin Enterprises

And

Larry Smith,

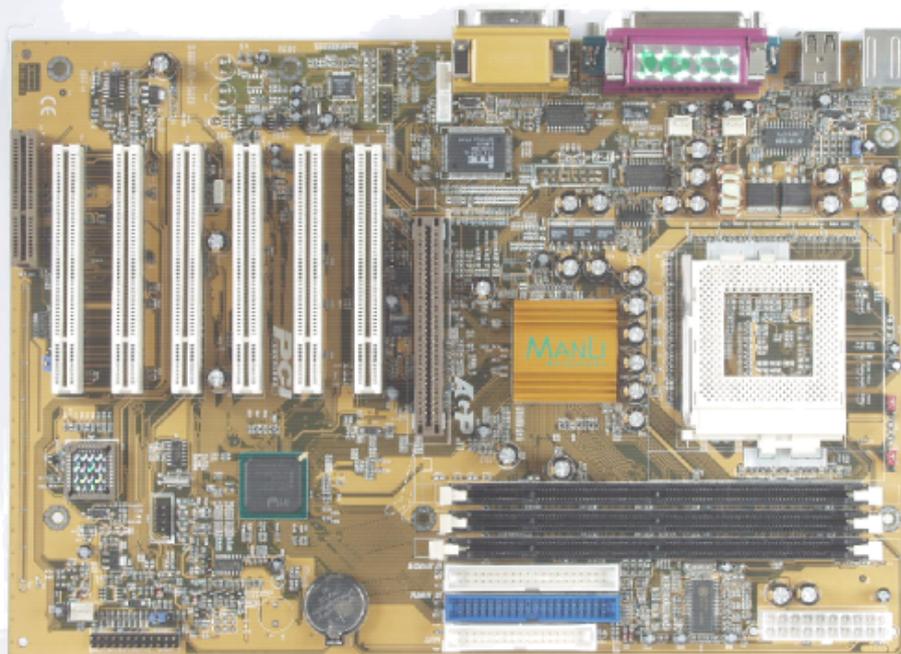
Signal Integrity Architect, Altera Corporation

Dec 9, 2009

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The Power Delivery Network

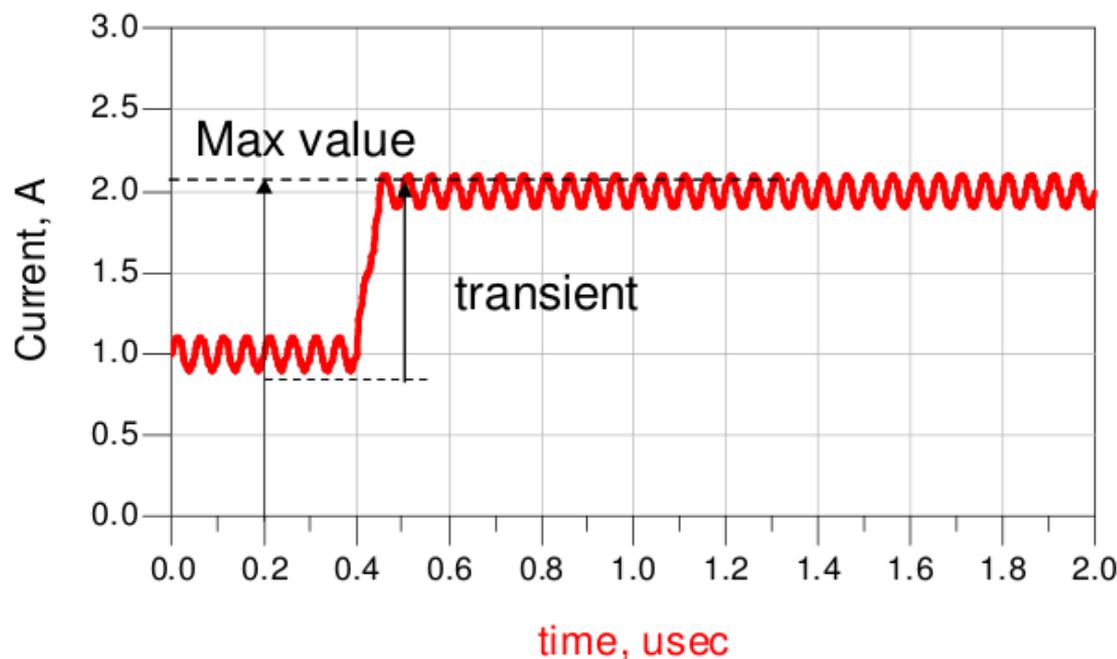


- All the interconnect from Voltage Regulator Module (VRM) to pads on the chip
- Purpose:
 - ✓ Provide stable voltage to chip pads from DC to $> BW$ of the signals
 - ✓ Provide low impedance return path for signals
 - ✓ To help mitigate EMI emissions

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1st Step: Estimate PDN Target Impedance



The diagram shows a red waveform representing a transient current pulse $I_{\text{transient}}$ above a horizontal line representing the PDN impedance Z_{PDN} . A double-headed arrow below the Z_{PDN} line indicates its extent.

$$V_{\text{PDN}} = Z_{\text{PDN}} \times I_{\text{transient}}$$

$$Z_{\text{PDN}} < \frac{V_{\text{dd}} \times \text{ripple}}{I_{\text{transient}}} = Z_{\text{target}}$$

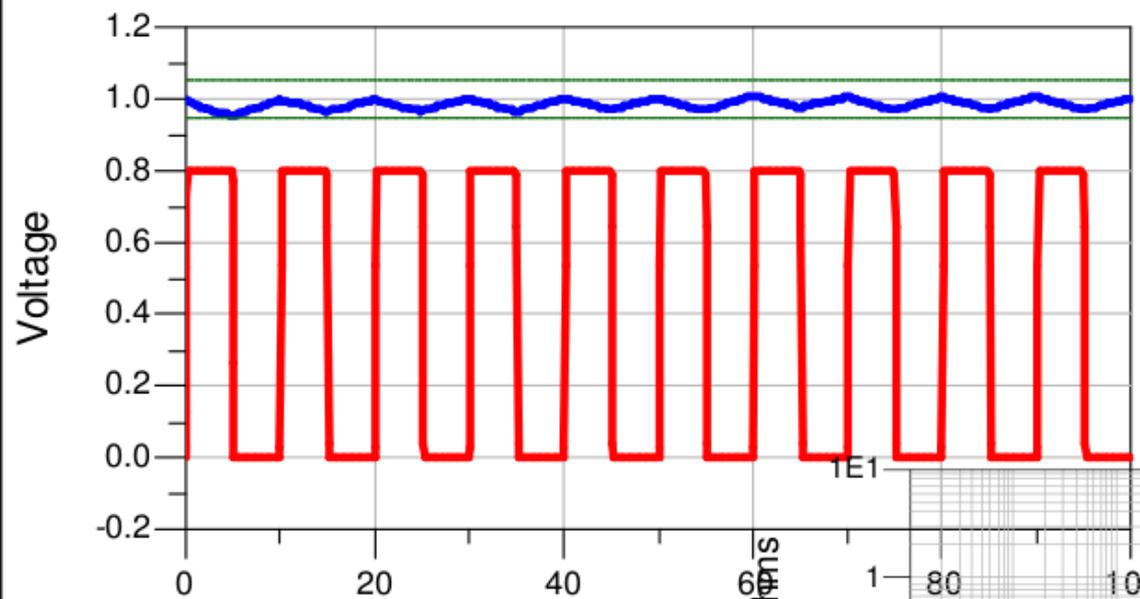
Example:
50 mV ripple noise
1 A transient current

$$Z_{\text{PDN}} \sim 50 \text{ mOhms}$$

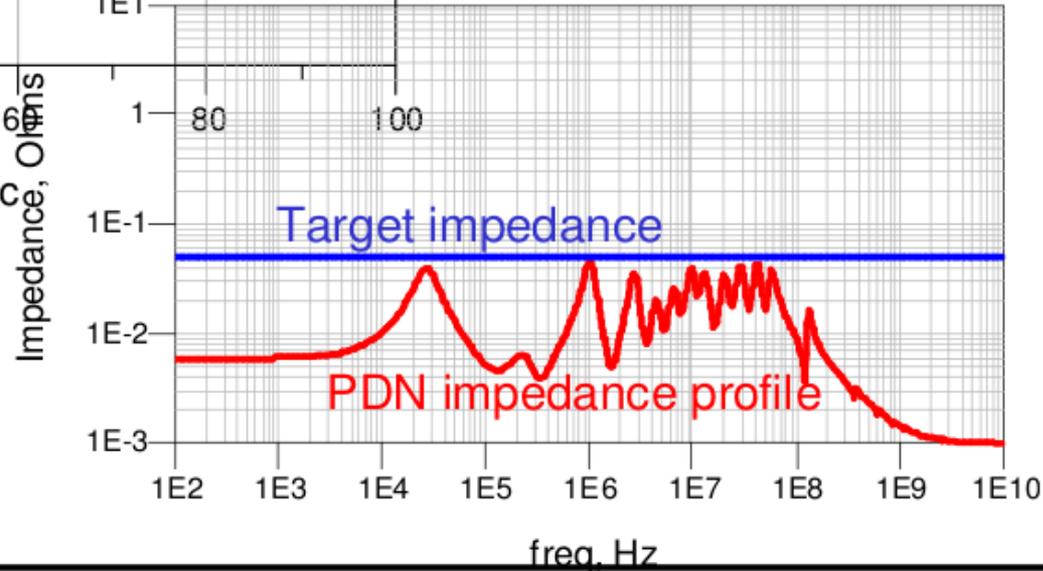
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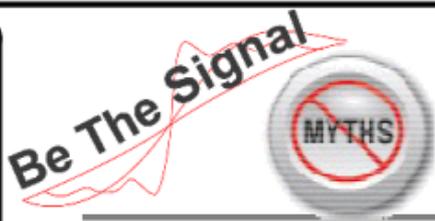


Goal: Keep PDN Impedance Below the Worst Case Target Impedance

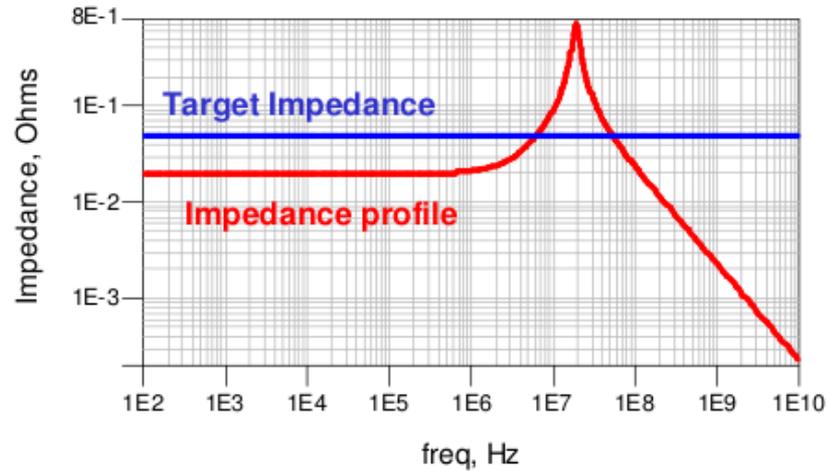


1 A transient current
 1 v Vdd
 ± 5% ripple spec
 Target impedance ~ 50 mOhm



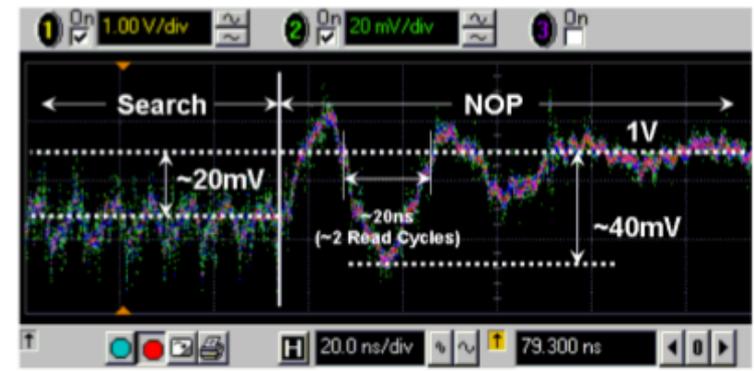
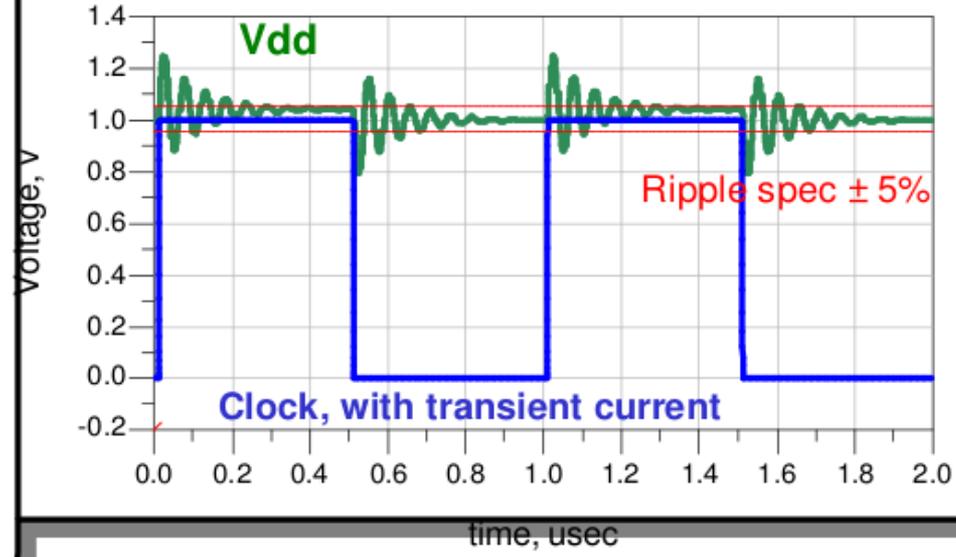


What if You Get it Wrong?



Golden Rule in PDN Design:

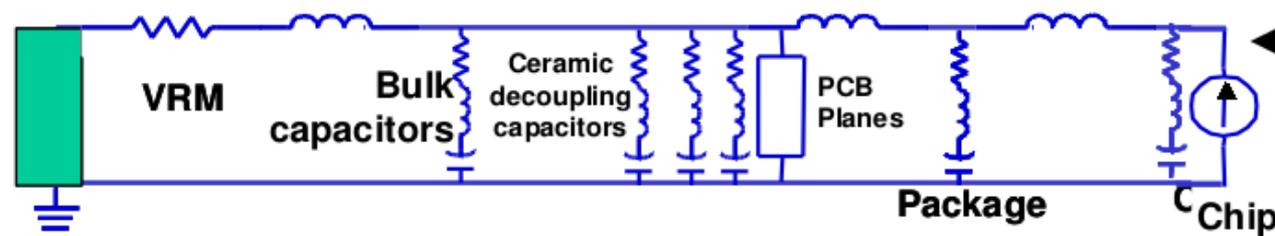
For robust PDN design, keep peak impedances below target impedance



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Elements of the PDN



- On-chip capacitance
- Package lead inductance and on package decoupling (OPD) capacitors
- Power and ground planes
- **MLCC (multi layer ceramic chip) capacitors**
- **Bulk tantalum, electrolytic capacitors**
- The voltage regulator module (VRM)

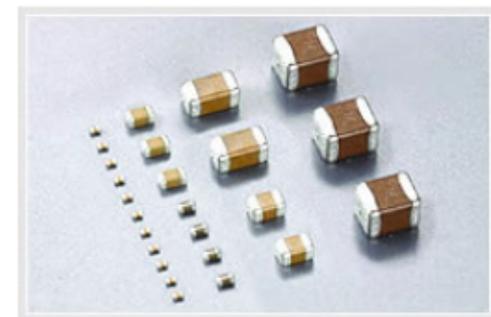
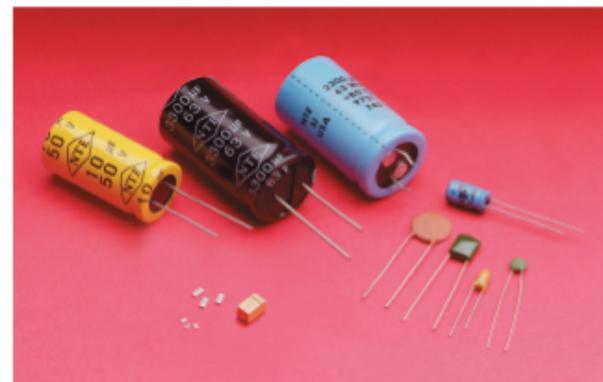


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How Many and What Value Capacitors to Use?

- ***It depends!***
- First order factors:
 - ✓ Target impedance
 - ✓ VRM equivalent inductance
 - ✓ On-die capacitance (ODC)
 - ✓ Package lead inductance, on-package decoupling (OPD) capacitance
 - ✓ Capacitor mounted inductance
- Second order factors
 - ✓ Power and ground plane capacitance
 - ✓ Planes' spreading inductance
 - ✓ Capacitor placement



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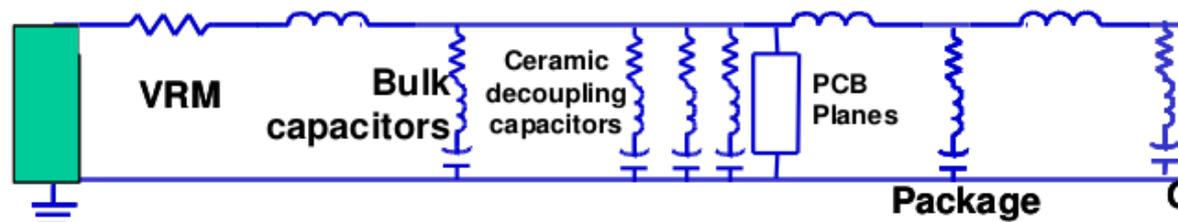


Approach #2

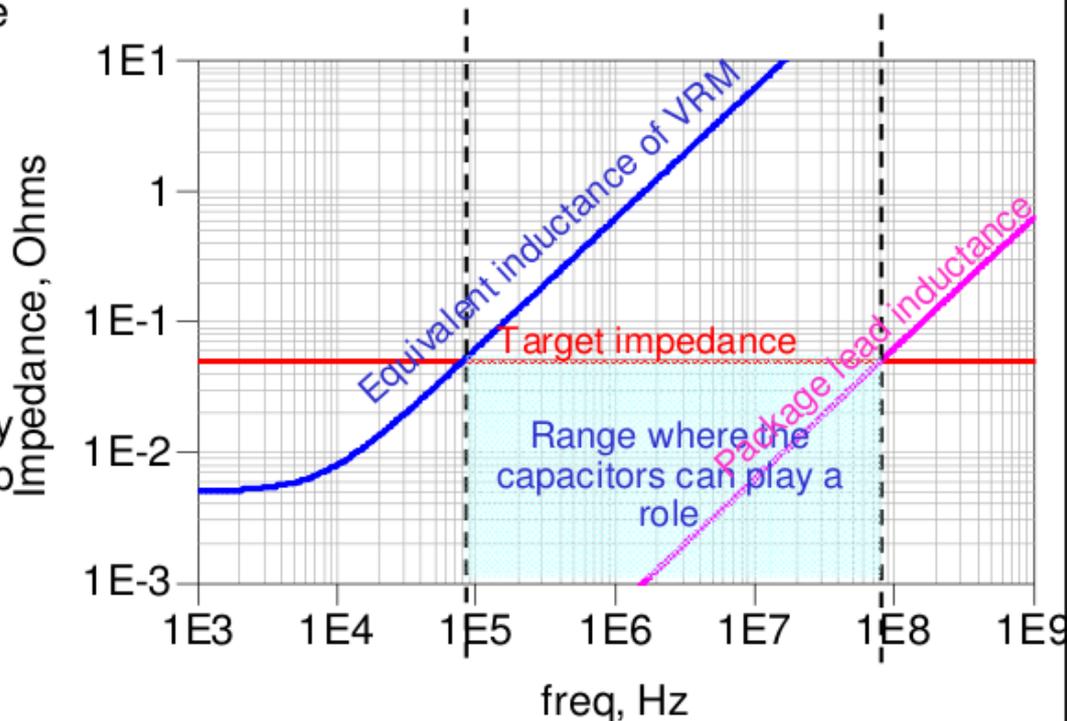
- Do your own analysis
 - ✓ Get the important starting information
 - ✓ Do a first order estimate
 - ✓ Add in second order factors
 - ✓ Do everything possible that is free
 - ✓ Use analysis tools to evaluate performance (SPICE, Agilent ADS, Altera PDN tool, Mentor PDN Analysis tool)
 - ✓ Select capacitor values and numbers based on impedance profile
 - ✓ Buy insurance by adding design margin
 - ✓ Use each design as an opportunity to move farther up the learning curve
 - ✓ The more you know, the luckier you get



BEFORE You Can Intelligently Select Capacitor Values:

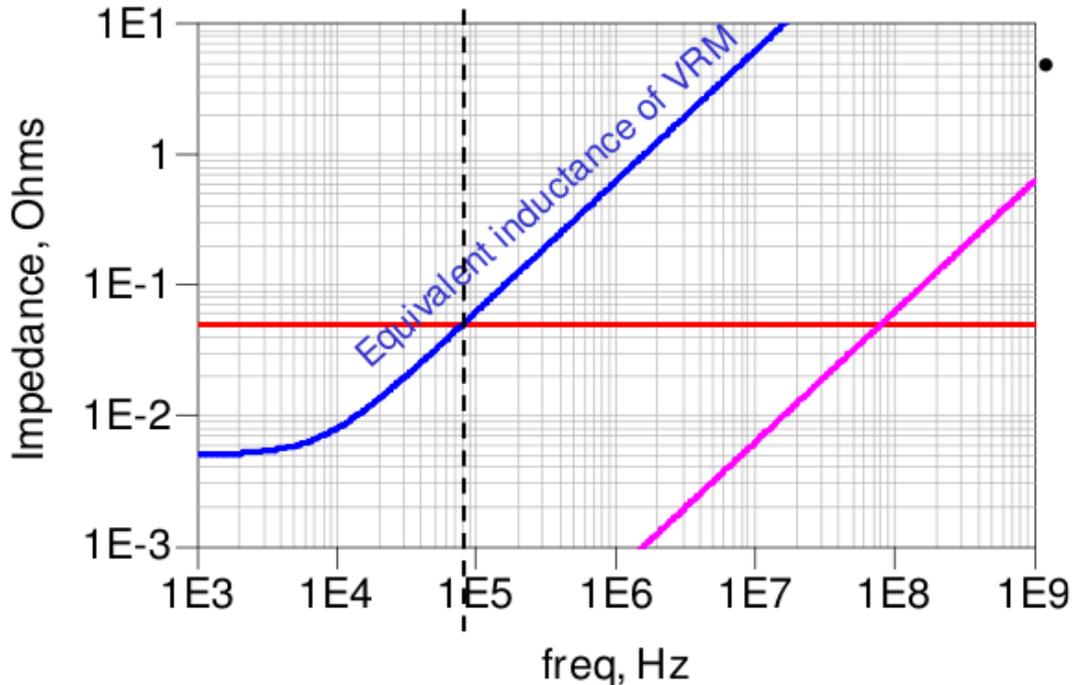


- ✓ Step 1: establish target impedance (based on transient current and noise spec)
- ✓ Step 2: establish the highest frequency where chip will see the board (based on package lead inductance)
- ✓ Step 3: establish the low frequency end where VRM is not able to keep the PDN impedance below the target impedance
- ✓ Defines 1st order goal: $Z_{cap} < 50$ mOhms, from 80 kHz to 80 MHz





Select Enough Bulk Capacitance for Low Frequency



- Select enough bulk capacitance so impedance is below target where regulator does not work

$$Z_C < Z_{target}$$

$$\frac{1}{(\omega C)} < Z_{target}$$

$$C > \frac{0.16}{f_{min} \times Z_{target}}$$

$f_{min} = 80 \text{ kHz}$

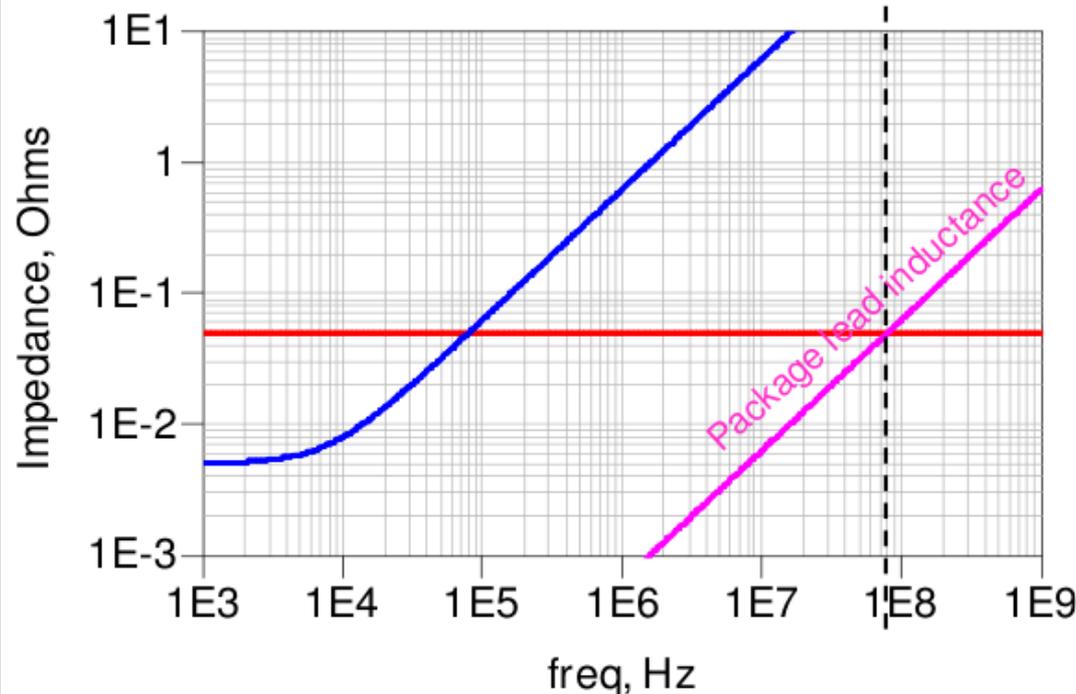
$Z_{target} = 50 \text{ mOhms}$

$$C > \frac{0.16}{0.08 \times 0.05} = 40\mu\text{F}$$

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High Frequency Limit and Target Impedance Define Maximum Equivalent L



$$Z_C < Z_{\text{target}}$$

$$\omega L_{\text{equiv}} < Z_{\text{target}}$$

$$L_{\text{equiv}} < \frac{0.16 \times Z_{\text{target}}}{f_{\text{max}} [\text{GHz}]}$$

$$f_{\text{max}} = 80 \text{ MHz}$$

$$Z_{\text{target}} = 50 \text{ mOhms}$$

$$L_{\text{equiv}} < \frac{0.16 \times 0.05}{0.08 [\text{GHz}]} = 0.1 \text{ nH}$$

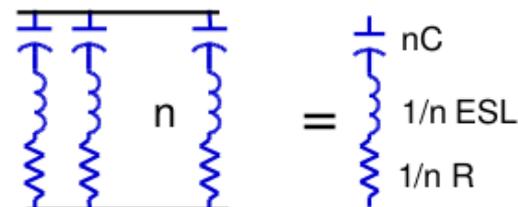
Comparable to the package lead inductance

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First Order Analysis Summary

- Starting place
 - ✓ Target impedance = 50 mOhms
 - ✓ VRM frequency limit = 80 kHz
 - ✓ Package high freq limit = 80 MHz
- Enough capacitance for low freq
= 40 uF
- Low enough inductance for high
freq = 0.1 nH
 - ✓ Hard to achieve with 1 capacitor
 - ✓ Use multiple in parallel:



$$n = \frac{ESL}{L_{\max}}$$

If ESL = 5 nH, n = 50

If ESL = 2 nH, n = 20

The ESL of the capacitors directly affects the cost of the PDN!



The ESL of the Capacitor Attach Affects the Minimum Number of Capacitors

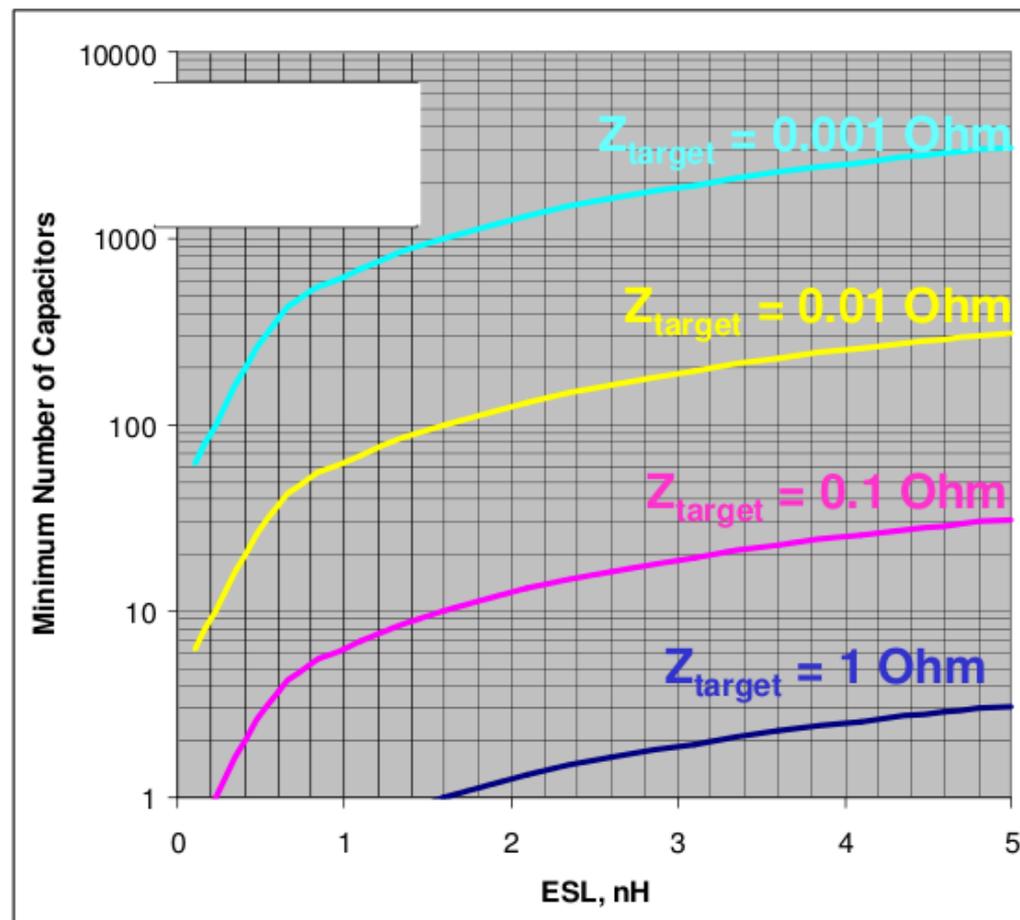
$$n > \frac{ESL \times f_{\max} [\text{GHz}]}{0.16 \times Z_{\text{target}}}$$

Assume $f_{\max} = 100 \text{ MHz}$

@ ~ 1¢/cap, this translates into cost savings per nH

The lower the ESL, the fewer the capacitor needed, the lower the cost

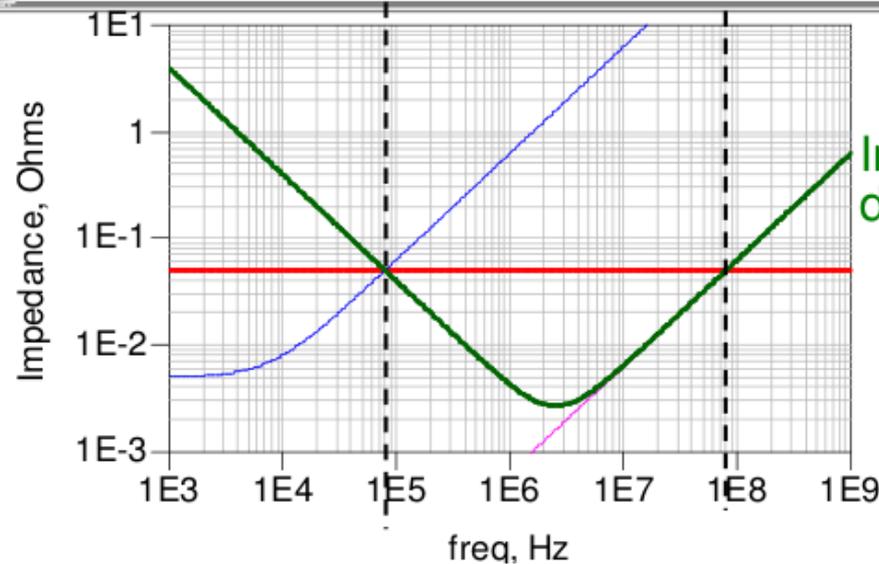
10 mOhm target, ESL ~ 1.5 nH
cost of PDN caps = \$1



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Result of First Order Analysis



Impedance of the decoupling capacitors

- Equivalent capacitance of 40 μF , equivalent inductance of 0.1 nH (20 @ 2 nH each)
 - ✓ Meets first order requirement!
 - ✓ We're done!
- ...Welcome to the real world:
 - ✓ Interaction with the VRM
 - ✓ Interaction with the package L and on-die C
 - ✓ Interaction with the planes

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Leveraging the High ESR of Smaller Capacitors to Damp Parallel Resonances at High Frequency

Specific Case:

ODC = 100 nF

$L_{pkg} = 0.1$ nH

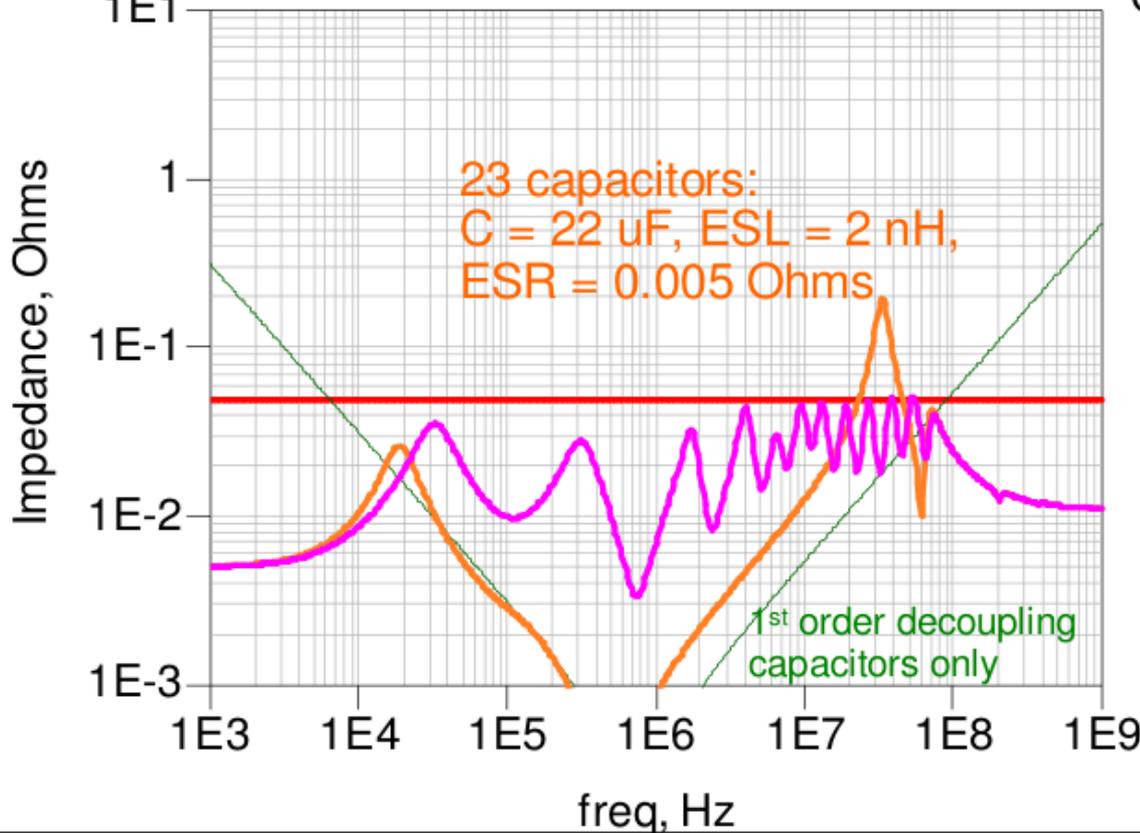
ESL = 2 nH

1E1

Estimated theoretical minimum number of capacitors: 20

Parallel resonant peak impedance

$$Z_{peak} \sim \frac{\left(\frac{1}{n}ESL + L_{pkg}\right)}{C_{chip}} \left(\frac{1}{\frac{1}{n}ESR + R_{pkg} + R_{chip}} \right)$$



C nF	n
22000	1
2200	1
470	1
220	1
100	1
47	2
22	3
10	5
4.7	8
Total	23

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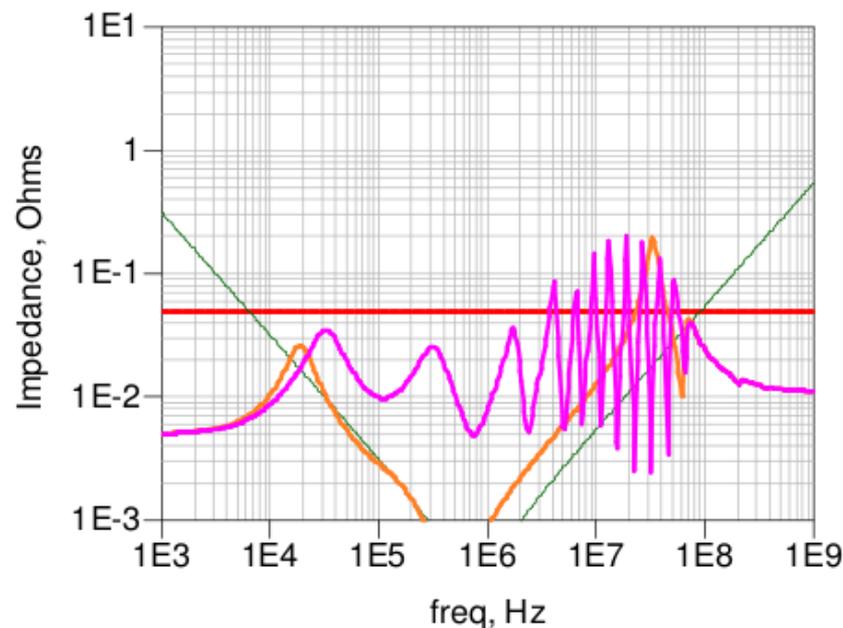
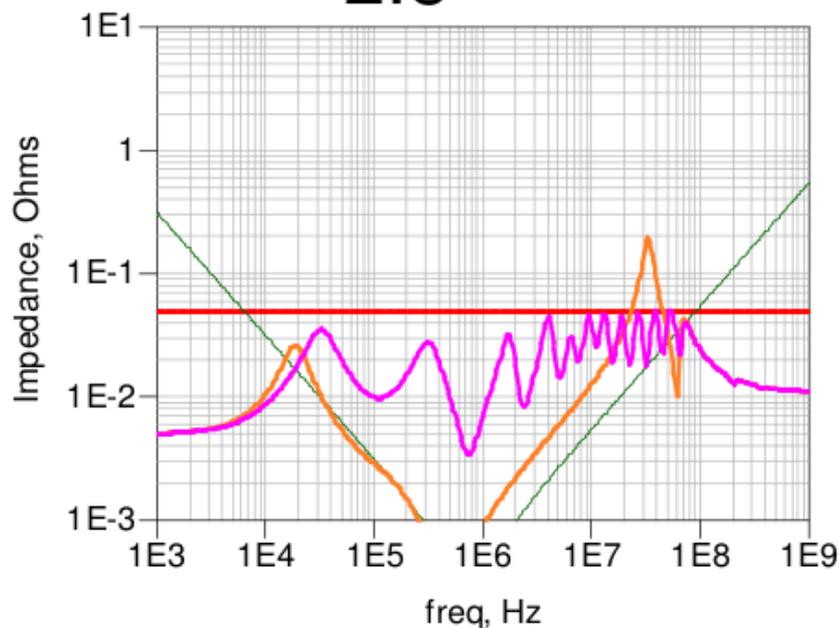
Impact of the Capacitor's ESR

Use multiple capacitor values:

1. Reduces peak impedance
2. Smaller C values have higher ESR

$$ESR \approx \frac{180m\Omega}{2.5^{\log(C)}} \quad C \text{ in nF}$$

$$ESR = 0.005 \text{ Ohms}$$



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Strategy to Select Capacitor Values

- Use bulk capacitor for low frequency to minimize parallel impedance with VRM
- Minimize capacitor mounting inductance by design
 - ✓ Use thin dielectric between power and ground planes (reduces spreading inductance)
 - ✓ Use multiple vias per capacitor (reduces spreading inductance)
 - ✓ Stack power and ground cavity as close to surface as possible
 - ✓ Use shortest, widest surface traces between capacitors and vias
 - ✓ Know what it is!
- Include:
 - ✓ ESL, Target impedance, On-die capacitance, Package lead inductance
- Select smallest capacitor body size practical
 - ✓ Use simulation (free SPICE, Agilent ADS, Mentor HyperLynx PI, Altera PDN tool)
 - ✓ Start with largest capacitor value, 1 value per decade, then 3 values per decade
 - ✓ Adjust n to bring peak impedance below target impedance

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Summary

• 1st order analysis

- ✓ Enough capacitance for low frequency
- ✓ Enough total number of capacitors for high frequency
- ✓ Lower ESL is ALWAYS a good thing- fewer capacitors, more robust design

• 2nd order analysis

- ✓ Optimize capacitor values to minimize parallel resonances
- ✓ Leverage the higher ESR of small capacitors

• Other factors

- ✓ When mounting inductance is small, spreading inductance in planes can be important- location matters
- ✓ IDC capacitors (like x2y) can significantly reduce mounting inductance

